

SCIENTIFIC REPORT

on the implementation of the project during January – December 2022 (stage 2)

The research team who carried out research activities in the project “Data-driven fuzzy control with experimental validation”, project number 192 / 19.02.2021, registration code PN-III-P4-ID-PCE-2020-0269, is the one nominated in the funding application form: Prof.Dr.Eng. Radu-Emil Precup (project leader), Assoc.Prof.Dr.Eng. Claudia-Adina Bojan-Dragoş, Assoc.Prof.Dr.Eng. Adriana Albu, Lect.Dr.Eng. Alexandra-Iulia Szedlak-Stînean, Lect.Dr. Ciprian Hedrea, Assist.Lect.Dr. Raul-Cristian Roman, M.Sc.Eng. Ion-Cornel Mituleţu, Phd student, Assist.Lect.Dr. Elena-Lorena Hedrea.

This research report is posted at https://www.aut.upt.ro/~rprecup/RS_PCE_2022.pdf.

A. PROGRESS SUMMARY

The results expected to be obtained during this stage of the project according to the funding application form are:

- The publication of one paper in a high impact leading journal and the participation and presentation of two papers to important conferences.
- Preparing the reports for the documentation of the activities.

The main results obtained in this stage of the project exceed the expected results. These are:

- The research report.
- A PhD thesis successfully finalized and defended by a member of the research team: Ms. Eng. Elena-Lorena Hedrea defended in September 1, 2022, the PhD Thesis “Tensor Product-based Model Transformation Used in Control System Modeling and Design”, PhD supervisor: Prof.Dr.Eng. Radu-Emil Precup. The PhD committee gave the thesis the Excellent qualification. The thesis contains chapters connected with the main objective of this project.
- 21 published papers: [C1]-[C21].
- Details on the published papers: 6 papers [C1]-[C6] published in journals indexed in Clarivate Analytics Web of Science (with one of the former names ISI Web of Knowledge) with impact factor, 4 papers [C7], [C8], [C10], [C11] published in conference proceedings indexed in Clarivate Analytics Web of Science (with one of the former names ISI Web of Knowledge or ISI Proceedings), 8 papers published in conference proceedings indexed in international databases (IEEE Xplore, INSPEC, Scopus, DBLP), 1 book published in Editura Politehnica, 2 book chapters published in Springer and World Scientific.
- The cumulative impact factor of the published papers according to 2021 Journal Citation Reports (JCR) published by Clarivate Analytics in 2022 = 38.843.
- High impact leading journals in which the papers were published: IEEE Transactions on Fuzzy Systems, International Journal of General Systems (Taylor & Francis), Information Sciences (Elsevier), Expert Systems with Applications (Elsevier).
- Important conferences in whose proceedings the papers were published: 2022 IEEE 31st International Symposium on Industrial Electronics ISIE 2022, 2022 IEEE International Conference on Fuzzy Systems FUZZ-IEEE 2022, 6th IFAC International Conference on Intelligent Control and Automation Sciences ICONS'22, 2022 IEEE Conference on Control Technology and Applications CCTA 2022, 48th Annual Conference of the IEEE Industrial Electronics Society IECON 2022, 2022 IEEE Symposium Series on Computational Intelligence SSCI 2022, 9th International Conference on Information Technology and Quantitative Management ITQM 2022.

THE EXECUTIVE SUMMARY OF THE PERFORMED ACTIVITIES IN THE IMPLEMENTATION STAGE

The main objective of the project was fulfilled according to the funding application form:

(2) The analysis, the design, the implementation and the validation of new Data-Driven Control (DDC) and Fuzzy Control (FC) algorithms through experiments made on several laboratory equipment also including Shape Memory Alloy (SMA) actuators and through cooperation with our external partners. The performed activities are 2.1, 2.2, 2.3 and 2.4:

2.1. The analysis of the actual stage of the research concerning the possibility of designing new DDC and FC algorithms used for improving the performance of the control system structures. The analysis was conducted and the brief results along with the corresponding references are presented in Chapter B.

2.2. Ensuring the desired control performance for the control system structures with controllers designed using DDC and FC algorithms and also ensuring the stability of these structures using stability criteria. The results of a stability analysis are presented in Chapter B. New controllers were analyzed and designed such as: fuzzy controllers [C1], [C5], [C6], [C9], [C10], [C11], [C19], [C20], [C21], Iterative Feedback Tuning-based controllers [C8], Active Disturbance Rejection Control, Model-Free Adaptive Control and Model Free Control-based controllers [C12], tensor product model transformation-based controllers [C16], artificial neural networks combined with reinforcement learning and metaheuristic optimization algorithms [C4] (details given in the published papers).

2.3. The design, testing and validation of new control system structures with controllers designed using DDC and FC algorithms through real time experiments conducted on several laboratory equipment including SMA processes. The processes and the equipment on which the design, testing and validation of the new control system structures were conducted are: servo systems [C1], [C4], [C5], [C12], tower crane systems [C6], [C8], [C9], [C10], [C16], big data systems [C7], SMA systems [C11], [C12], and magnetic levitation systems [C19]. Many preparations were made concerning the development of new control system structures through the analysis of processes and derivation of models for systems such as: strip winding systems [C2], [C14], vertical three tank systems [C3], tower crane systems [C13], mobile robots [C15], [C18], brain-computer interfaces [C17], prosthetic hand [C20], electromagnetic actuated clutch systems [C19], continuously variable transmission vehicles [C19].

2.4. The validation of the new control system structures designed using DDC and FC algorithms with the support of the external partners (Continental Automotive Timisoara, Airbus Helicopters – through direct timely consolidated links, Ontario Centres of Excellence – through Prof. Emil M. Petriu, our Canadian partner, Centre of Autonomous and Cyber-Physical Systems of Cranfield University, UK – a fresh cooperation with Dr. Argyrios Zolotas, and ECU Security Research Institute, Australia – through the Project Leader and his colleagues from Edith Cowan University). Due to the pandemics, the experiments at the external partners could not be conducted. However, many experiments were conducted in the laboratories of the research team and the published papers contain the simulation and real-time experimental results obtained with the support of the external partners. These results concern the algorithms and models from the papers whose co-author is Prof. Emil M. Petriu, our partner from Canada: [C1], [C2], [C4], [C8]–[C11], [C13]–[C15] and the book [2] published in 2021 in CRC Press, Taylor & Francis with our external partner Dr. Ali Safaei from Canada. Three of the controllers are in the validation stage, to be finalized in 2023, at Continental Automotive Timișoara (the partnership was created in 2008-2011 through the project PCCA “Real-time informatics technologies for embedded-system-control of power-train in automotive design and applications (SICONA)”, project leader, Prof.Dr.Eng. Corneliu Lazăr, Technical University “Gheorghe Asachi” of Iași; the partnership was materialized, among others, with a testing stand) and at the company from Canada where Dr. Ali Safaei works. Due to privacy and non-competition reasons, the results cannot be published. However, in the research report from in there will be presented minimal information on the processes on which the controllers designed by the research team were tested and the results obtained at the external partners. For protecting the algorithms proposed in this project, the design methodologies and the corresponding source programs of three Data-Driven Control, Fuzzy Control and Data-Driven Fuzzy Control algorithms will be registered in the National Register of Works handled by the Romanian Office for Copyright (ORDA) in 2023. In 2022 the contract of the project leader as Adjunct Professor at Edith Cowan University (Australia, 2016-2022) has ended; therefore, the connections with Australia weakened. However, the research team started the cooperation with a team from the University of Craiova for developing new fuzzy controllers for discrete events systems; the cooperation started with the published paper [C3] and the team from Craiova has good connections with external partners in the region.

Remarks:

1. In this scientific report the texts, the figures and partially the equations were taken from the papers developed by the research team. This is the reason why the formulations are in English. For some of the equations the numbering will be kept in the research report.
2. All published papers and papers currently in publication, which contain research results obtained in this project, mentioned the support of UEFISCDI in the Acknowledgements section, along with specifying the project registration code from the funding application form.
3. Some of the papers specified in Chapter C contain more than one project in the Acknowledgements section. Several projects contributed in the process of creating these papers because the same processes were controlled but using different controllers designed in different projects. Therefore, the fair comparison of all recent designed controllers was necessary.

B. SCIENTIFIC AND TECHNICAL DESCRIPTION

The description is focused on the synthetic presentation of the research carried out in the framework of the activities 2.1 and 2.2.

As specified in this project proposal (application form) and the paper [C5], also given in Section C as [1], in contrast to model-based control, data-driven control avoids the system (process) identification by constructing controllers directly from data. That is the reason why data-driven control is also referred to as model-free control (i.e. no model in controller tuning), justifying the high interest in nonlinear controllers whose parameters are tuned using process input-output data after conducting few experiments, or, more generally, data-driven model-free control [2]. Instead, one or more experiments are conducted in order to use the information in controller tuning, and non-parametric system or process models) can be employed in this regard.

A concise discussion on the popular data-driven control techniques is given in Precup et al. [3] pointing out the following ones that ensure the iterative experiment-based update of controller parameters: Iterative Feedback Tuning (IFT) [4], [5], Model-free Adaptive Control (MFAC) [6], [7], Simultaneous Perturbation Stochastic Approximation [8], [9], Correlation-based Tuning [10], [11], Frequency Domain Tuning [12], [13], Iterative Regression Tuning [14], and adaptive online IFT [15]. A review on data-driven control [16] offers classifications and highlights the role of observers and estimation in control, also leading to non-iterative data-driven control techniques: Model-Free Control (MFC) [17], [18], Virtual Reference Feedback Tuning (VRFT) [19], [20], Active Disturbance Rejection Control (ADRC) [21], [22], data-driven predictive control [23], [24], unfalsified control [25], [26], Data-Driven Inversion Based Control [27], [28], and the investigation of equivalent conditions on the given data under which different analysis and control problems can be solved [29]. Other representative techniques are emphasized in book [2]. It is suggestively stated in [3] and [30] that MFC is an efficient tool for Machine Learning; moreover, as specified earlier in [25], unfalsified control is also an efficient tool for Machine Learning.

As pointed out in the studies conducted in [1] and [31], fuzzy control is an important subject in the area of nonlinear control as the fuzzy controllers are relatively easily understandable and also offer very good control system performance indices. However, the heuristic approach to design and tune fuzzy controllers is compensated by the systematic design of fuzzy controllers that can employ the stable design of fuzzy control systems, the optimal and robust controller design and tuning. Classical and recent applications of fuzzy control deal with Popov-type stability analysis [32], embedded fuzzy control system for machining processes [33], tire slip control [34], predictive functional control based on fuzzy models [35], stability and sensitivity analysis of fuzzy control systems [36], stability analysis dedicated to the fuzzy control of nonlinear processes [37], robust evolving cloud-based control [38], power control of series hybrid electric vehicles [39], vehicle navigation by fuzzy cognitive maps [40], fuzzy control for the iron ore sintering process [41], type-2 fuzzy control for line following [42], and singularity-free fixed-time fuzzy control for robotic systems [43].

The model-free tuning of fuzzy controllers is an alternative approach to the model-based design resulting in data-driven fuzzy control [1] to benefit from the advantages of data-driven control and fuzzy control and to mitigate their drawbacks. The combinations of data-driven model-free and fuzzy control

include H_∞ fuzzy control [44], fault tolerant fuzzy control [45], parameterized data-driven fuzzy control [46], data-driven interpretable fuzzy control [47], MFC merged with Proportional-Derivative (PD) Takagi-Sugeno fuzzy control [48], [49], MFAC merged with PD Takagi-Sugeno fuzzy control [50], [51], ADRC mixed with PD Takagi-Sugeno fuzzy control [52] and tuned by VRFT [22] as well, fuzzy logic-based adaptive ADRC [53], data-driven arithmetic fuzzy control using the distending function [54], and data-driven MFC developed around continuous-time intelligent Proportional-Integral (PI) control [31]. The indirect model-free tuning of fuzzy controllers has initially been proposed in authors' papers [55] and [56], and continued in [48] and [50] by controller structures that combine data-driven control and fuzzy control in order to incorporate model-free features in fuzzy control system structures. However, it is preferred to use the term "data-driven fuzzy control" instead of "model-free fuzzy control" because non-parametric models are actually used in controller tuning in several model-free control techniques.

The Model-Free Control (MFC) approach will be presented as follows along with stability analysis results in terms of the useful information given in [2] in the continuous time case. MFC is a data-driven technique that uses the input/output data of the control process in the controller design, it uses the online linear approximation of the process and an estimator to update the linear approximation [Fli13], [Rom16b], [Rom18c].

The control algorithms tuned by MFC, also known as MFC algorithms, are well-known in the state-of-the-art as "intelligent" controllers or MFC controllers to highlight the controllers that are implemented based on the MFC technique, usually designed based on Proportional (P), Proportional-Integral (PI) or Proportional-Integral-Derivative (PID) type controllers. The MFC controllers that contain P, PI, or PID elements are also known as intelligent P, PI and PID controllers, with the abbreviations iP, iPI and iPID, respectively. The MFC technique is also known in the literature as model-free tuning [Fli13], [Rom18c]. Within the MFC-based tuning the parameters of the controllers, non-parametric mathematical models of the processes can be used in the form of process responses to various input signals, i.e. control signals [Fli13], [Rom16b], [Rom18c].

The MFC algorithm uses an ultra-local model $\mathbf{y}^{(v)} = \mathbf{F} + \boldsymbol{\alpha} \mathbf{u}$ to replace the unknown mathematical model of the process, where the controlled output (i.e. the process output) vector $\mathbf{y}^{(v)}(t)$ is the v^{th} order derivative of \mathbf{y} with $v \geq 1$ ($v=1$ in the case of first order MFC algorithm, and $v=2$ in the case of the second order MFC algorithm), \mathbf{u} is the control input vector or the control signal vector, the vector \mathbf{F} plays a disturbance role that is continuously updated, and $\boldsymbol{\alpha}$ is a constant matrix.

The iPID controllers are PID controllers equipped with an online parameter estimation method for estimating the unknown nonlinear or linear dynamics of the controlled system. In this regard, their structure is generally similar to PID controllers, while estimated parameters of the system are included.

The theory of iPID controllers for continuous-time dynamic systems is focused as follows on the description of the structure of iPID controllers for continuous-time dynamic systems offered in [2].

Definition 1. The dynamics of a generic system is defined as follows [Fli13]:

$$\dot{\mathbf{y}} = \mathbf{F} + \mathbf{B} \mathbf{u}, \quad (1)$$

where $\mathbf{y} \in \mathfrak{R}^n$ is the system output (or the controlled output) vector, $\mathbf{u} \in \mathfrak{R}^n$ is the system input (the control signal or the control input) vector, $\mathbf{F} \in \mathfrak{R}^n$ is representing the entire nonlinear dynamics of the system, $\mathbf{B} \in \mathfrak{R}^{n \times n}$ is the input matrix of the system, and n is the number of system inputs and outputs, i.e. supposed to be equal. The structure defined in (1) is known as *ultra-local* model for a generic dynamic system. In general case, \mathbf{F} and \mathbf{B} are assumed unknown.

Theorem 1 [2]. For the ultra-local model defined in *Definition 1*, the iPID controller is defined as

$$\mathbf{u} = \hat{\mathbf{B}}^{-1}(\dot{\mathbf{y}}_d - \hat{\mathbf{F}} + \mathbf{v}), \quad (2)$$

where $\mathbf{v} \in \mathfrak{R}^n$ is the regular PID term of the controller (see *Remark 1* given as follows), $\mathbf{y}_d \in \mathfrak{R}^n$ is the reference input vector (or the set-point vector or the desired set-points for system outputs). The term \mathbf{v} is proposed based on the control error $\mathbf{e} \in \mathfrak{R}^n$, i.e. the output tracking error vector of the system, which is defined in terms of

$$\mathbf{e} = \mathbf{y}_d - \mathbf{y}. \quad (3)$$

Proof. Here, the proof is presented in the generic case of a PID controller for \mathbf{v} but it can also be generalized to the other definitions pointed out in this proof. Let us define the following Lyapunov

function candidate:

$$V = \frac{1}{2} \mathbf{e}^T (\mathbf{I}_n + \mathbf{k}_d) \mathbf{e} + \xi^T \mathbf{k}_i \xi, \quad (4)$$

where $\xi = \int \mathbf{e} dt$ and $\mathbf{I}_n \in \mathfrak{R}^{n \times n}$ is an identity matrix. Then, the first time-derivative of this function is

$$\dot{V} = \mathbf{e}^T \dot{\mathbf{e}} + \mathbf{e}^T \mathbf{k}_d \dot{\mathbf{e}} + \mathbf{e}^T \mathbf{k}_i \xi. \quad (5)$$

Replacing $\dot{\mathbf{e}}$ in the first term on the right-hand side of (5), the relations (3) and (1) lead to

$$\dot{V} = \mathbf{e}^T (\dot{\mathbf{y}}_d - \mathbf{F} - \mathbf{B} \mathbf{u}) + \mathbf{e}^T \mathbf{k}_d \dot{\mathbf{e}} + \mathbf{e}^T \mathbf{k}_i \xi. \quad (6)$$

Now, utilizing

$$\dot{\mathbf{y}}_d - \mathbf{F} + \mathbf{k}_p \mathbf{e} + \mathbf{k}_i \xi + \mathbf{k}_d \dot{\mathbf{e}}, \quad (7)$$

we reach at

$$\dot{V} = -\mathbf{e}^T \mathbf{k}_p \mathbf{e} \leq 0. \quad (8)$$

Based on the *Lyapunov* stability theorem [Kha02], since $V > 0$ and $\dot{V} \leq 0$, then \mathbf{e} will be asymptotically stable and converge to zero. Moreover, by replacing \mathbf{F} and \mathbf{B} in (6), with their corresponding estimated vector variables and parameters $\hat{\mathbf{F}}$ and $\hat{\mathbf{B}}$, the controller given in (2) will be achieved. The usage of the estimated variables are permissible according to the *separation principal* [Ata99], if these estimated variables are computed utilizing stable observers (or state estimators). This completes the proof.

Remark 1 [2]. The term \mathbf{v} in (2) is defined as follows for a regular P controller:

$$\mathbf{v} = \mathbf{k}_p \mathbf{e}, \quad (9)$$

for a regular PI controller is

$$\mathbf{v} = \mathbf{k}_p \mathbf{e} + \mathbf{k}_i \int \mathbf{e} dt, \quad (10)$$

for a regular PD controller is

$$\mathbf{v} = \mathbf{k}_p \mathbf{e} + \mathbf{k}_d \dot{\mathbf{e}}, \quad (11)$$

and finally for a regular PID controller is considered as

$$\mathbf{v} = \mathbf{k}_p \mathbf{e} + \mathbf{k}_i \int \mathbf{e} dt + \mathbf{k}_d \dot{\mathbf{e}}. \quad (12)$$

Here, $\mathbf{k}_p \in \mathfrak{R}^{n \times n}$ is the proportional controller gain matrix, $\mathbf{k}_i \in \mathfrak{R}^{n \times n}$ is the integral controller gain matrix and $\mathbf{k}_d \in \mathfrak{R}^{n \times n}$ is the derivative controller gain matrix.

Remark 2 [2]. As it is observed in (2), the estimated parameters and vectors of the dynamic system, i.e. $\hat{\mathbf{F}}$ and $\hat{\mathbf{B}}$, are incorporated into the iP controller. This is the basic feature of all model-free controllers. The values of $\hat{\mathbf{F}}$ and $\hat{\mathbf{B}}$ should be estimated online, in order to implement the proposed iP controller in (2). The different approaches to this online parameter estimation problem are presented in [2].

Remark 3 [2]. In (2), the time-derivative of the desired system output vector, i.e. $\dot{\mathbf{y}}_d$, is required in the controller. In order to provide correctness and robustness into the differentiation process and consequently into the controlled system, the sliding mode differentiator [Lev03] is suggested to compute $\dot{\mathbf{y}}_d$ as follows:

$$\dot{\mathbf{y}}_d = \boldsymbol{\eta}, \quad (13)$$

where for $\boldsymbol{\eta} = [\eta_1 \quad \eta_2 \quad \dots \quad \eta_n]^T$ the following relationships hold [Lev03]:

$$\begin{aligned} \dot{w}_i &= \eta_i, \\ \eta_i &= -k_1 \sqrt{|w_i - y_{di}|} \operatorname{sgn}(w_i - y_{di}) + \tau_i, \\ \dot{\tau}_i &= -k_2 \operatorname{sgn}(w_i - y_{di}), \end{aligned} \quad (14)$$

for $i = 1 \dots n$, where $\operatorname{sgn}(\cdot)$ is the sign function.

Iterated time integrals for online parameter estimations and Adaptive observers for online parameter estimations are thoroughly investigated in [2]. The theory is again backed up by the Lyapunov

stability theorem.

References of Section B

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